

# LONG TERM DEVELOPMENT STATEMENT

## FOR SCOTTISH HYDRO ELECTRIC POWER DISTRIBUTION PLC'S ELECTRICITY DISTRIBUTION SYSTEM

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MAY 2024



Scottish & Southern  
Electricity Networks



# SCOTTISH HYDRO ELECTRIC POWER DISTRIBUTION PLC LONG TERM DEVELOPMENT STATEMENT

## FOREWORD

Scottish Hydro Electric Power Distribution plc (SHEPD) is pleased to present this Long-Term Development Statement (LTDS) for its electricity distribution network. It is produced by SHEPD in accordance with its Electricity Distribution Standard Licence Condition (SLC) 25. The statement covers the period 2022/23 to 2027/28.

The main purpose of the LTDS is to assist existing and prospective users of the electricity distribution network in assessing opportunities available for making new connections, or for additional use of the SHEPD distribution system.

The assets referred to in this document are in the ownership of Scottish Hydro Electric Power Distribution plc which delivers electricity to over 785,000 customers in Scotland.

Although all reasonable efforts have been made to ensure the accuracy of data, SHEPD does not accept any liability for the accuracy of the information contained herein and in particular neither SHEPD, nor its directors or employees, shall be under any liability for any errors.

This document may not be reproduced, in whole or part, for any purpose, without the written consent of Scottish Hydro Electric Power Distribution plc.

# CONTENTS

<b>INTRODUCTORY SECTION .....</b>	<b><u>4</u></b>
1 PURPOSE OF STATEMENT .....	4
2 CONTENTS OF STATEMENT .....	4
3 CONTACT DETAILS .....	6
4 OTHER INFORMATION SOURCES .....	7
<b>SUMMARY INFORMATION .....</b>	<b><u>28</u></b>
1 GUIDING PRINCIPLES FOR PLANNING THE DISTRIBUTION SYSTEM.....	9
2 STANDARDS .....	9
3 DESIGN POLICIES .....	13
4 NETWORK CHARACTERISTICS .....	15
5 GEOGRAPHIC AND SCHEMATIC PLANS .....	23
6 SOURCES OF NETWORK AND CHARGING INFORMATION.....	24
<b>DETAILED INFORMATION.....</b>	<b><u>28</u></b>
7 DETAILED INFORMATION.....	25
8 NETWORK DEVELOPMENT PROPOSALS .....	26
9 UPCOMING CHANGES TO THE FORM OF THE LTDS .....	27
10 FURTHER INFORMATION .....	29
APPENDIX 1 .....	30
APPENDIX 2 .....	32
APPENDIX 3 .....	33



# INTRODUCTORY SECTION

## 1 PURPOSE OF STATEMENT

This Long Term Development Statement (LTDS) is prepared in accordance with Standard Licence Condition 25.

The purpose of this statement is to:

- Provide sufficient information which will assist existing and prospective new users who are contemplating entering into distribution arrangements with the licensee, to identify and evaluate opportunities.
- Ensure the general availability of such information in the public domain.
- Inform users of distribution network development proposals.
- Provide users of the correct point of contact for specific enquiries.

Users of the distribution system should also be aware that the main document which governs development and operation of the distribution system is the Distribution Code. This code covers all material technical aspects relating to connections to and the operation and use of the distribution systems of the Licensee.

## 2 CONTENTS OF STATEMENT

This LTDS is in two parts.

- Part 1 gives an overview of document content and provides relevant contact details and sources of information.
- Part 2 contains detailed information of the system.

The statement contains a range of information associated with our 33 kV distribution system including the 11 kV busbar of 33/11 kV primary substations.

Information relating to 11 kV and LV systems may be available on request depending on the area. A price list for the provision of this data is included in Appendix 1.

Part 2 of the statement gives:

- Detailed information on the guiding principles for planning the distribution system, company internal standards, design policies and network characteristics.
- Schematic and geographical plans showing the 33 kV system including location of 132/33 kV and 33/11 kV substations.
- Details of embedded generation.
- Planned network development proposals for which financial approvals have been given in Appendix 3. They provide a summary of the work to be carried out, timescale and area of the network impacted by each proposal. These exclude like for like replacement (as this does not change system capability) and system developments for new or existing users.

- Detailed information relating to:
  - Circuit Data, Table 1
  - Transformer Data, Table 2
  - Demand Data\*, Table 3
  - Fault Level Data\*, Table 4
  - Generation Data, Table 5
  - Connection Interest Table 6
  - Schematic Diagrams of the Distribution Network Single Line Diagrams

\* Demand forecast methodology is formulated around a combination of important contributing factors impacting demand. Historic growth rates for each primary substation are calculated before being banded into four growth trends of Zero, Low, Medium, or High.

Individual future growth rates are based on the calculated historic trend and key drivers including committed connections, geographic economic factors derived from local authority development plans and demand forecast from large users with knowledge of major changes in connected load.

The key assumptions included in the demand forecast are as follows:

- Exponential growth is assumed and calculated using historic maximum demand readings over the past five years.
- Consistent running arrangement and system configurations are considered. Recorded substation peak demands are normalised to account for abnormal running arrangements or equipment faults to ensure the forecast is consistent to previous years running arrangement.
- Power export from distributed generators (DG) is removed, where possible, from recorded figures to give a true representation of underlying substation demand.
- Individual demand forecast submissions from large consumers are factored into forecasts
- Committed new loads and new connections are assumed to materialise in the manner predicted i.e., user timing and usage is assumed to occur as advised/requested by customer.
- Future Zero growth rates are assumed to have a forecast trend of 100% i.e., neither increasing nor decreasing.

\* SHEPD will undertake further assessments to determine whether intervention is required where the calculated planning fault levels, identified in Table 4, exceed 95% of the circuit breaker fault level rating. The additional assessments undertaken by SHEPD include, but are not limited to, site specific protection settings analysis and circuit breaker trip testing.

If further assessments confirm that intervention is required SHEPD will determine the most economic, efficient and cost-effective solution to reduce the overall fault level. Possible mitigation works include, but are not limited to, opening the bus-section circuit breaker, reconfiguring the network, installing fast response automation, and extending circuit breaker trip times.

Details of the 132 kV system (regarded as transmission voltage in Scotland) are included in the Electricity Ten Year Statement, which is available on National Grid's Electricity System Operator website.

<https://www.nationalgrideso.com/>

### 3 CONTACT DETAILS

The LTDS is available free of charge by sending an email to:

[Modelling.Reporting@sse.com](mailto:Modelling.Reporting@sse.com)

or by making a request through the Scottish and Southern Electricity Networks website:

<https://www.ssen.co.uk/our-services/tools-and-maps/long-term-development-statements-ltds/>

For further information relating to LTDS, or to provide feedback:

Modelling & Reporting  
Scottish Hydro Electric Power Distribution plc  
Inveralmond House  
200 Dunkeld Road  
Perth  
PH1 3AQ  
E-mail: [Modelling.Reporting@sse.com](mailto:Modelling.Reporting@sse.com)

Enquiries relating to new load connections or changes to existing load connections should be addressed to:

Connections and Engineering  
Customer Service Centre  
Scottish and Southern Electricity Networks  
Walton Park, Walton Road  
Cosham, Portsmouth  
PO6 1UJ  
E-mail: [connections@sse.com](mailto:connections@sse.com)  
Tel: 0800 0483516

Enquiries relating to connection of generators should be addressed to:

Major Connections Contracts (MCC)  
Scottish and Southern Electricity Networks  
Perth Training Centre  
Ruthvenfield Way  
Inveralmond Industrial Estate  
Perth  
PH1 3AF  
E-mail: [mcc@sse.com](mailto:mcc@sse.com)  
Tel: 0345 0724319

Enquiries relating to connection of generators should review the options on the Scottish and Southern Electricity Networks website:

<http://www.ssen.co.uk/GenerationConnectionsHome/>

Enquiries relating to the provision of copies of the “Statement of methodology and charges for connection” should be addressed to:

Connections Policy Team  
Scottish Hydro Electric Power Distribution plc  
Inveralmond House  
200 Dunkeld Road  
Perth  
PH1 3AQ  
Email: [connections.policy@sse.com](mailto:connections.policy@sse.com)

The Connection and Use of System charging statements can be viewed on our website. Our connection charging statements are revised from time to time and our Use of System charging statements are revised at least annually. Revised Use of System charges normally take effect from 1 April of each year. The latest documents can be viewed via the link below:

<http://www.ssen.co.uk/Library/ChargingStatements/SHEPD/>

## 4 OTHER INFORMATION SOURCES

### **Distributed Generation Connection Guide**

The ENA produces connection guides to help users as an owner or developer of distributed generation to connect distributed generation to the UK’s electricity distribution networks.

The guides can be viewed by following the link below:

<https://www.energynetworks.org/operating-the-networks/connecting-to-the-networks>

### **Guaranteed Standards**

In accordance with the Electricity (Standards of Performance) Regulations 2015, DNOs are obliged to meet guaranteed standards of performance set by OFGEM, the industry regulator.

These guaranteed standards are laid out in three documents which can be viewed by following the below links:  
The Guaranteed Standards:

- The Electricity (Connection Standards of Performance) Regulations 2015

[http://www.legislation.gov.uk/uksi/2015/698/pdfs/ukxi\\_20150698\\_en.pdf](http://www.legislation.gov.uk/uksi/2015/698/pdfs/ukxi_20150698_en.pdf)

Part 2 – Services and Standards for Metered Connections

Part 3 – Services and Standards for Unmetered Connections

- The Electricity (Standards of Performance) Regulations 2015

[http://www.legislation.gov.uk/uksi/2015/699/pdfs/ukxi\\_20150699\\_en.pdf](http://www.legislation.gov.uk/uksi/2015/699/pdfs/ukxi_20150699_en.pdf)

- The Electricity and Gas (Standards of Performance) (Suppliers) Regulations 2015

[http://www.legislation.gov.uk/ukxi/2015/1544/pdfs/ukxi\\_20151544\\_en.pdf](http://www.legislation.gov.uk/ukxi/2015/1544/pdfs/ukxi_20151544_en.pdf)

### Process to Request Additional Network Data

Enquiries relating to the provision of additional network data to that contained in the LTDS should be sent to:

[Modelling.Reporting@sse.com](mailto:Modelling.Reporting@sse.com)

### SSEN Data Portal

In October 2023, we launched our Data Portal to drive forward net zero decisions. Our Data Portal is a single point of access to all the data SSEN publishes and a catalogue of data that brings visibility to our network assets, their location, their usage, and their performance. All documents related to the SHEPD and SEPD LTDS submission are published on our Open Data Portal, along with other planning publications such as the Network Development Plan, DFES, Capacity Heatmaps and Embedded Capacity Register (ECR). The timeline of these documents is shown in the figure below.

SSEN Distribution’s commitment to transparency and accessibility is a significant step forward in the transition to a net-zero future, and by providing this vital information, this data portal will play a pivotal role in reducing greenhouse gas emissions, improving energy efficiency, and ultimately taking us all closer to achieving our sustainability goals.

We have built our data portal on CKAN allowing us to display our data in a user-friendly environment and allow our data consumers to use data in a meaningful way. CKAN has been used extensively by our Open Data Peers and Partners and allows us to tailor our portal, to serve our customers.

Link to data portal: [SSEN Data Portal](#). To understand how to use our portal please view our video guide [here](#).

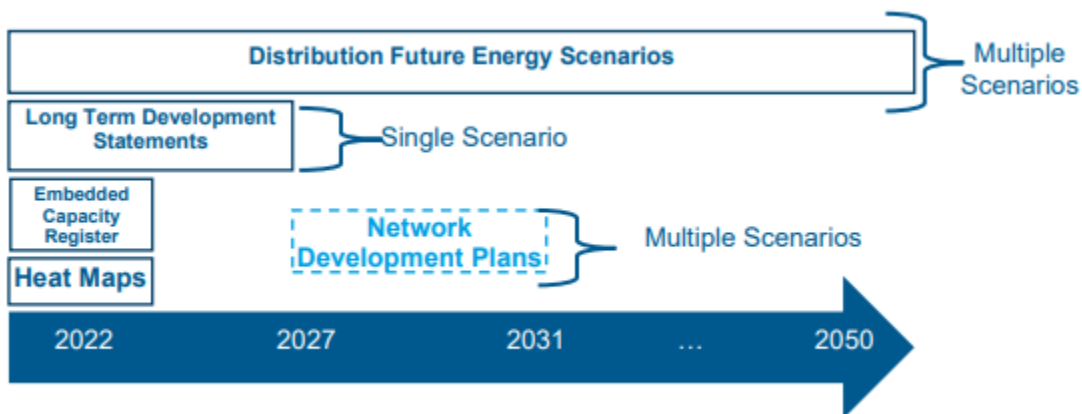


Figure 1 - LTDS in relation to other scenario and capacity reporting by DNOs



# SUMMARY INFORMATION

## 1 GUIDING PRINCIPLES FOR PLANNING THE DISTRIBUTION SYSTEM

The following standards are the guiding principles which underpin the policy for planning and designing the distribution network in Scottish Hydro Electric Power Distribution plc:

Licence Conditions

Distribution Code

Electricity Safety, Quality and Continuity Regulations

Environmental Standards

Company Internal Standards

## 2 STANDARDS

### 2.1 Licence Conditions

**2.1.1** Pursuant to a licensing scheme made by the Secretary of State, under part II of Schedule 7 to the Utilities Act 2000, Scottish Hydro Electric Power Distribution plc has been granted a licence under section 6(1) (c) of the Electricity Act 1989 authorising it to distribute electricity for the purpose of giving a supply to any premises in the area specified in Schedule 1 of the Act.

**2.1.2** Standard Licence Condition (SLC) 24 – Distribution System Planning and Quality of Supply sets out the requirement for licensees to plan and develop their distribution system to a certain standard. SHEPD meets this requirement by having an Ofgem approved planning standard (TG-NET-NPL-012 Distribution Planning – Standards of Voltage and Security of Supply) which sets out how security of supply will be met in its distribution services area.

In order to meet the above standard our policy is to plan networks at the most economic cost. To achieve this, we have taken two approaches:

For high volume works where point of connection is low voltage (230 and 400 V) or high voltage (11 kV) we have standard connection arrangements which ensure compliance with Engineering Recommendation P2/8.

For lower volume, high cost developments, principally at 33 kV and above, we will tailor development to meet standards on an individual basis to optimise cost-benefit and customer requirements.

**2.1.3** Under SLC 12 - Requirement to Offer Terms for Use of System and Connection, the licensee shall, on application, offer to enter into an agreement (Connection Agreement) for use of system.

Where the licensee makes an offer to enter into a connection agreement, the licensee shall, in making the offer, make detailed provision regarding:

The carrying out of the works required to connect the licensee's distribution system to any other system for distribution of electricity.

The carrying out of works in connection with the extension or reinforcement of licensee's distribution system rendered appropriate by reasons of making the connection.

Installation of such switchgear or other apparatus (if any) as may be required for the interruption of supply where the person seeking connection or modification of an existing connection does not require the provision of top-up or standby.

The charges to be paid in respect of services required. For the purpose of determining an appropriate proportion of the costs directly or indirectly incurred the licensee shall have regard to the benefit to be obtained or likely in the future to be obtained.

In determining the costs of connection of demand and generation, the licensee shall apply the charging principles set out in the annual charging statements including, where applicable, application of:

Cost apportionment of any necessary reinforcement for the Connection; and  
Distributed Generation Incentives.

The statements which set out the basis of charges for "Use of System" and "Connection to the Distribution System" are entitled:

Scottish Hydro Electric Power Distribution plc's Use of System Charging Statement;

Statement of Methodology and Charges for Connection to Scottish Hydro Electric Power Distribution plc's Electricity Distribution System.

(all the above are amended as required)

All the above statements are available on our website [www.ssen.co.uk](http://www.ssen.co.uk) or by sending an email to [connections@ssen.co.uk](mailto:connections@ssen.co.uk).

Note: Some distribution connected generators will have impact on the transmission system (typically where the generator's authorised export capacity is either greater than 10 MW and / or is more than the declared summer minimum demand at the 33 kV busbar of the relevant 132/ 33 kV substation). Such generators may be liable for transmission use of system charges (TNUoS) from National Grid Electricity System Operator (NGESO). Prospective generators seeking a distribution connection should also consult NGESO under BETTA (British Electricity Trading and Transmission Arrangements), to assess the impact their generation project may have on the GB transmission system.

## **2.2 Distribution Code**

Under SLC 20 of the Licence the licensee shall prepare and at all times have in force and shall implement and comply with the Distribution Code.

The Distribution Code covers all material technical aspects relating to connections to and the operation and use of the licensee's distribution system or the operation of electric lines and electrical plant connected to the licensee's distribution system.

It requires the licensee's distribution system to be designed so as to permit the development, maintenance and operation of an efficient, co-ordinated and economical system and to facilitate competition in the generation and supply of electricity.

The Distribution Code includes:

A distribution planning and connection code containing:

- Connection conditions specifying the technical, design and operational criteria to be complied with by any person connected or seeking connection to the licensee's distribution system; and

- Planning conditions specifying the technical and design criteria and procedures to be applied by the licensee in the planning and development of the licensee's distribution system and to be taken into account by persons connected or seeking connection with the licensee's distribution system in the planning and development of their own plant and system; and

A distribution operating code specifying the conditions under which the licensee shall operate the licensee's distribution system and under which persons shall operate their plant and/or distribution systems in relation to the licensee's distribution system, in so far as necessary to protect the security and quality of supply and safe operation of the licensee's distribution system under both normal and abnormal conditions.

It contains references to the following Electricity Supply Industry publications which provide guidance on planning and design criteria:

- **Engineering Recommendation G5/5**  
Planning levels for harmonic voltage distortion and the connection of harmonic sources and/or resonant plant to transmission systems and distribution networks in the United Kingdom.
- **Engineering Recommendation G12/4**  
Requirements for the application of protective multiple earthing to low voltage networks.
- **Engineering Recommendation P2/8**  
Security of Supply.
- **Engineering Recommendation P24**  
AC supplies to railway systems.
- **Engineering Recommendation P25**  
The short-circuit characteristics of single-phase and three-phase low voltage distribution networks.
- **Engineering Recommendation P28**  
Planning limits for voltage fluctuations and the connection of disturbing equipment to transmission systems and distribution networks in the United Kingdom.
- **Engineering Recommendation P29**  
Planning limits for voltage unbalance in the United Kingdom for 132kV and below.
- **Technical Specification 41-24**  
Guidance for the design, installation, testing and maintenance of main earthing systems in substations.
- **Engineering Recommendation S34**  
A guide for assessing the rise of earth potential at substation sites.
- **Engineering Recommendation G98**  
Requirements for the connection of Fully Type Tested Micro-generators (up to and including 16 A per phase) in parallel with public Low Voltage Distribution Networks.
- **Engineering Recommendation G99**  
Requirements for the connection of generating equipment in parallel with public distribution networks.

See Section 9 for enquiries relating to the Distribution Code.

## 2.3 Electricity Safety, Quality and Continuity Regulations

The Secretary of State issued The Electricity Safety, Quality and Continuity Regulations in 2002 in order to:

Ensure that the electricity supplies are regular and efficient.

Protect the public from dangers arising from distribution of electricity, use of electricity supplied or from installation, maintenance or use of any electricity line or electrical plant.

Eliminate or reduce the risks of personal injury or damage to property or interference with its use.

Regulation 27 gives permitted variations at all low voltage customers' terminals of +10% and -6% of the declared voltage of 230 V single phase or 400 V three phase. For 33 kV the permitted variations are between +6% and -6% of the declared voltage. It is therefore necessary to hold the system voltage within these ranges on all systems to which customers are connected, i.e. all low voltage systems, most 11 kV systems and some 33 kV systems.

## 2.4 Environmental Standards

Schedule 9 of the Electricity Act 1989 requires SHEPD to consider the effect of its work on the amenity and fisheries and to mitigate the effects where reasonable.

In planning, designing and operating the distribution system our policy is to pay due regard to environmental matters and, in particular, noise, visual amenity and pollution. We seek Planning Authority and Scottish Ministers' approval to build new lines. We also endeavour to meet the requirements of other bodies in protected areas such as National Scenic Areas. We will seek to avoid disturbance or detriment to such areas as far as reasonably practicable consistent with the economic and reliability impact on our distribution network and on customers' costs.

## 2.5 Company Internal Standards

In addition to meeting the above standards, SHEPD has internal standards to improve quality of supply and reduce duration of supply interruptions.

### 2.5.1 General

The targets for duration of supply interruption, customer minutes lost (CMLs) per customer per year, and number of customer interruptions (CIs) are agreed with Ofgem. These standards are in addition to the Guaranteed Standards set by Ofgem.

In planning, designing and operating the distribution system the systematic use of automation, mobile generation and targeted investment for refurbishment of the distribution system is designed to deliver these targets.

To meet the individual needs of customers, we will agree standards of connection whether in excess or lower than the appropriate levels as stated in the relevant network standard. In these cases, we will agree special commercial terms.

### 2.5.2 Capacity Planning

To ensure that the distribution system has adequate capacity to meet system demand, voltage and current flows are regularly monitored and adequacy of the network is checked. Capacity is benchmarked to estimated loads. Where there is a shortfall in network capacity we will seek appropriate solutions. These will usually involve network reinforcement but could involve alternative solutions.

### 2.5.3 System Voltage Control

The total full load volt drop for the transfer of power from the high voltage distribution system to the low voltage supply system is approximately 30%. Therefore, voltage correction must be applied in the appropriate places to comply with Regulation 27 of the Electricity Safety, Quality and Continuity Regulations 2002. This is carried out as follows:

At transmission voltages by National Grid:

- Control of reactive power flows. This includes switching in or out lightly loaded circuits, shunt capacitors and reactors, use of synchronous compensators, operation of "tap-stagger" and use of voltage above or below nominal.
- Auto or manually controlled on-load tapchangers on 275/132 kV transformers .
- Central control by despatch of reactive power from synchronous generators.
- Automatic voltage control on synchronous generators.

At distribution voltage levels by:

- Automatically controlled on-load tapchangers fitted to 132/33 kV and 33/11 kV transformers (some smaller < 1 MVA 33/11 kV transformers have off-load tap changers);
- Automatically controlled on-load tapchangers fitted to 33 kV, 11 kV and LV voltage regulators;
- Line drop compensation on some rural 11 kV systems;
- Automatic voltage control on embedded generators;
- Reactive compensation (fixed & variable tap shunt reactors, fixed shunt capacitors and DSTATCOMs);
- Off load tap changers fitted to 33 kV/LV and 11 kV/LV transformers.

## 3 DESIGN POLICIES

### 3.1 General

When planning and designing an electricity distribution system it is necessary to consider all alternative options to achieve an optimum solution based on technical and economic considerations.


The Company's distribution system has been standardised at 33 kV, 11 kV and 230/400 V (called LV).

### 3.2 132 and 33 kV System Design

33 kV networks from 132/33 kV substations normally run either radially or as open or closed rings. However, some networks run in parallel with those from other sources where technically acceptable and economically advantageous.

Additions to or reinforcements of these networks are considered individually and tailored to the existing network arrangements. The most economic investment is determined in line with any long term proposals and having regard to network complexity, operational requirements and flexibility.

Studies are completed to ensure acceptable voltage conditions, compliance with security of supply standards for first and second circuit outages and that circuit and plant ratings are not exceeded.



Additionally, for generation, studies are completed to identify any locations where increased fault currents exceed switchgear ratings. For larger sets, or where there is likely to be interaction with existing customers with large motor drives, steady state and transient stability studies are needed to ensure generation and the network remain stable following circuit switching or a network fault.

Check interaction with other nearby generation.

Predict any possible loss of synchronism and the corresponding need for additional protection to avoid damage to the generator or unacceptable voltage or power swings.

### **3.3 Supplies from 33/11 kV Substations**

The maximum number of 11 kV circuits from a 33/11 kV substation is determined on the basis of network configuration and maximum utilisation e.g. for a substation with 2 x 12/24 MVA transformer capacity normal maximum number of 11 kV feeders would be 7.

Interconnecting feeders, where practical, would emanate from separate sections of busbar consistent with minimising initial switchgear requirements and allowing for future extensions.

Feeders will be controlled by automatic circuit breakers of 630 A nominal load rating. Many existing circuit breakers have nominal load rating of 400 A or less.

### **3.4 11 kV Network Configuration**

The 11 kV network is normally configured to achieve maximum utilisation whilst maintaining security of supply standards at a minimum cost.

The 11 kV urban network is normally configured as a "loop-tee-loop" arrangement in an open "ring" formation. However, where an individual customer requires more or less security of supply standard, then the connection to that customer will be designed to meet specific needs.

The 11 kV rural network is normally configured as an open "ring" with pole mounted 11 kV/LV transformers directly connected. However, where group demand is below 1 MVA the network configuration may be radial feed with no backfeed facility.

Furthermore, there may be lengthy single phase and three phase spurs in particularly remote locations served by overhead line circuits.

### **3.5 Low Voltage Network Configuration**

The feeding arrangement on the low voltage network is normally radial with no interconnection. There is existing interconnected LV network which operates as radial and is configured as "open" ring. The layout of distributors is optimised in relation to services to be supplied. Distributors are normally laid in footways.

# 4 NETWORK CHARACTERISTICS

## 4.1 Standard Plant and Equipment sizes

Various types of plant and equipment exist on the 33 kV and 11 kV systems. Typical details are given below.

### 4.1.1 33 kV System

- Voltage Regulators
  - Vector Group Auto transformer
  - Voltage Ratio 33/33 kV
  - Rating Between 5 MVA and 32 MVA
  - Tapping Range -18% to + 4%
  
- Primary Transformers
  - Voltage Ratio 33/11 kV or 33/11.5kV (off load)
  - Vector Group: YY0
  - Rating: 1, 2.5, 4, 6.3 & 8 MVA ONAN 7.5/15, 10, 12/24, 15/30, 20/40 MVA CER
  - Tapping Ranges: -18% to +4% (on load) for 33/11kV or -15% to +11.67% (on load) for 33/11.5kV ONAN or -13.33% to +13.33% (on load) for 33/11.5kV CER
  - Rating: 0.1, 0.15, 0.2, 0.3, 0.5, 1.0, 1.5 MVA
  - Tapping Range: -5% to +5% (off-load).

Voltage Ratio 33 kV/LV (433V) (off load)

- Vector Group: DYn11
- Rating: 200, 500, 800, 1000, 1500 kVA (ground mounted)
- Tapping Range: -5% to +5% (off load)

Voltage Ratio 33 kV/LV (250 or 500V) (off load)

- Rating: 16, 25, 50, 100 kVA (pole mounted)
- Tapping Range: -5% to +5% (off load)

Switchgear

- Current Rating 400, 800, 1200, 1600, 2000, 2200, 2500 A
- Fault rating 8.7, 13.1, 17.5, 25, 31.5 kA

### 4.1.2 11 kV System

- Voltage Regulators
  - Vector Group Auto transformer
  - Voltage Ratio 11/11 kV
  - Rating Between 1 MVA and 8 MVA
  - Tapping Range -18% to + 4%
  
- Transformers
  - Vector Group: DYn11
  - Voltage Ratio: 11 kV/LV (433 V)

Ground Mounted

- Rating: 315, 500, 800, 1000, 1500 kVA
- Tapping Range -5% to 5% (off load).

Pole Mounted

- Rating 50, 100, 200 kVA
- Tapping Range -5% to 5% (off load).
- Transformers
- Voltage Ratio 11 kV/LV (250 or 500 V)
- Rating 16, 25, 50, 100 kVA (pole mounted)
- Tapping Range -5% to 5% (off load).

• Switchgear

- Current Rating 400, 630, 800, 1250, 2000 A
- Fault rating 13.1 or 18.4 kA - some pole mounted switchgear may be rated below 13.1 kA.

**4.1.4 Telecontrol**

Normally all 33 kV or higher voltage switchgear is equipped with telecontrol. Use of telecontrol at 11 kV is considered according to the situation and location.

**4.1.5 Batteries**

SHEPD will normally provide its own battery systems where required for distribution sub stations. However, shared use is considered if appropriate.

**4.2 Power Quality**

**4.2.1 Harmonics**

Engineering Recommendation G5/5 sets the planning levels for harmonic voltage distortion to be used for the connection of non linear equipment. These levels should not normally be exceeded when considering the connection of non linear loads and generating plant to the distribution networks under the Distribution Code. The table below gives a summary of Total Harmonic Distortion (THD) planning levels at supply system point of common coupling (PCC) nominal operating voltage:

Nominal Voltage (V) kV	THD Limit
LV ( $\leq 400$ V)	5%
HV ( $< 20$ kV)	4%
EHV ( $< 400$ kV)	3%

Table 1 – Total Harmonic Distortion Limits

The assessment procedure for non-linear equipment follows three stages:

Stage 1 facilitates the connection of harmonic sources to LV supply systems.

Stage 2 facilitates the connection of harmonic sources to all supply systems operating at a voltage of greater than LV and less than 33 kV, including any harmonic source that is too large for consideration under Stage 1, or that cannot meet the emission limits of Stage 1. Measurement of the background harmonic level may be required, before a simplified assessment is made of the predicted harmonic voltage level at the PCC that may result from the connection of the new harmonic source.

Stage 3 applies to the connection of the harmonic sources that are not found to be acceptable under Stage 2 assessment or which fall outside the scope of Stages 1 & 2, excluding Stage 2 assessments with an LV PCC. It also applies to any harmonic sources that have a nominal PCC voltage greater than or equal to 33kV and to the assessment of relevant plant where the connection is made at system voltages of 33kV or higher.



The objective is to balance the degree of detail with degree of risk that the connection of the particular equipment will result on the supply system.

#### **4.2.2 Voltage Fluctuations**

Engineering Recommendation P28 sets the planning limits of voltage fluctuations caused by industrial, commercial and domestic equipment. Allowable limits vary with the interval between fluctuations and are based on the likelihood of customer complaints. Normally acceptable values are 3% and below.

#### **4.2.3 Unbalance**

Engineering Recommendation P29 sets the limits of voltage unbalance on networks up to 132 kV. Normally acceptable values are 2% and below.

#### **4.2.4 Investigations**

There are no areas in SHEPD where harmonic levels, voltage fluctuations or unbalance are known to be an issue. However, we will investigate and take measurements in response to customer requests. If found to be unacceptable we will seek an appropriate solution.

### **4.3 Method of Earthing**

#### **4.3.1 Primary substations**

The methods currently employed to earth the neutral of High Voltage networks at primary (33/11kV) substations are:

##### Direct Earthing

The only impedance between the transformer lower voltage winding star point (neutral) and earth consists of the earthing conductor and the resistance between the earth mat and earth.

##### Resistance Earthing

Use is made of an earthing resistor between the transformer lower voltage winding star point (neutral) and earth to limit the earth fault current.

##### Matching Transformer

In some instances, where generation is connected to the transformer low voltage winding, the neutral is earthed by a single phase transformer with secondary load resistor to restrict fault current to low values.

##### Earthing Transformers

In instances where the transformer lower voltage winding is delta connected a neutral point is derived artificially by inclusion of an earthing transformer. This neutral point is then appropriately earthed.

In addition to the above Arc Suppression (Peterson) coils are also used in some cases. Furthermore, there are occasions where transformer high voltage winding is earthed (or provided with a selectable earth switch). This is where there is islanded generation or where there are subsea cables (for protection against overvoltage during faults).

#### **4.3.3 Distribution Substations**

Earthing is provided for HV metal work, LV neutral and extraneous metal work not associated with the power system e.g. fences etc.

Where the overall resistance to earth does not exceed 1 ohm the HV metal work, LV neutral earth and fence metal work (within 2 metres of HV metal work) are combined together. Where the overall resistance to earth exceeds 1 ohm HV metal work earth, LV neutral and fence metal work earths are kept separate and resistance to earth of each separate earth electrode must not exceed 40 ohms.

#### 4.3.4 Low Voltage System

The method applied to earth the LV system of most new networks and many existing networks is Protective Multiple Earthing (PME). This refers to the use of the supply neutral conductor of the LV network to provide earthing facilities for customers.

There is also use of Continuous Earth Wire, Separate Neutral and Earth and Protective Neutral Bonding systems.

The general requirements that must be fulfilled are:

The supply neutral conductor will be connected to an earth electrode at or near the transformer star point.

The supply neutral conductor will not contain a fusible cutout, circuit breaker or switch.

The value of the transformer neutral earth electrode will not exceed 40 ohms.

The overall resistance to earth of the supply neutral conductor will not exceed 20 ohms.

In addition to the neutral earth at or near the transformer star point, the supply neutral conductor will be connected to other points either to earth electrodes or supply neutral conductor of another distributing main.

#### 4.4 Protection Systems

##### 4.4.1 General

Protection equipment is used to recognise, locate and initiate removal of a fault or abnormal condition from the power system, normally by operation of a switching device. Circuit breakers and relays are normally used at higher voltages, but fuses are employed where relays are not economically justified.

To avoid unnecessary damage to plant and equipment and to minimise disconnection of healthy plant, it is essential that the protection systems employed on the distribution system are reliable, selective, fast and sensitive.

##### 4.4.2 LV Feeders

In most cases low voltage feeders are protected by fuses. These provide short circuit protection to the main feeder and connected services. The fuses are rated to provide discrimination with HV protection.

##### 4.4.3 11 kV/LV Transformers (Ground Mounted)

Ground mounted 11 kV / LV transformers are normally protected by HV fuse switches. The fuses provide protection for faults on the HV cable to the transformer, faults within the transformer and faults on the LV connections.

##### 4.4.4 11 kV/LV Transformers (Pole Mounted)

Pole mounted 11 kV / LV transformers receive protection from either feeder circuit breaker, pole mounted auto reclosers / sectionalisers or pole mounted HV fuses.

##### 4.4.5 11 kV Feeders

11 kV feeders are normally protected by circuit breakers with the following protections and typical clearance times:

Predominantly underground circuits:

- IDMT overcurrent and earth fault protection - up to 1 s, but possibly up to 3 s depending on fault type and location.

Predominantly overhead line circuits:

- Instantaneous high set overcurrent - 150 ms.
- IDMT overcurrent and earth fault - up to 1 s, but possibly up to 3 s depending on fault type and location.
- Time delayed sensitive earth fault - 7 s.
- Auto-reclosing as para. 4.6

Additional pole mounted auto reclosers are strategically located on the overhead network to limit the number of supply interruptions to customers for transient and permanent faults.

#### **4.4.6 33/11 kV Transformers**

33/11 kV transformers typically have the following protection and clearance times:

High set overcurrent, instantaneous earth fault and restricted earth fault – 150 ms.

3 stage standby earth fault - 1.4 s, 2.1 s and 2.9 s.

IDMT overcurrent and earth fault - up to 3 s.

Neutral voltage displacement protection - 3 – 10 s.

Buchholz and winding / oil temperature relays.

Intertripping or fault throwing switch if needed to trip remote circuit breaker – 300 ms or operating time of remote protection.

#### **4.4.7 33 kV Feeders and Transformer Feeders**

33 kV feeders are normally protected by circuit breakers fitted with protection dependent upon feeder type (overhead or underground cable). Typical protection provided (and clearance time) is a selection from:

Unit protection - 150 ms.

Distance protection - 150 ms zone 1, 500 ms zone 2, 1.3 s zone 3.

IDMT overcurrent and earth fault - up to 3s.

Auto-reclosing as para. 4.6 for predominately overhead circuits.

Additional protection is needed if remote transformers are connected, typically:

High set overcurrent - 150 ms.

Instantaneous earth fault - 150 ms.

Intertripping over pilot cable or fault throwing switch.

#### **4.5 Network Automation**

In order to minimise customer minutes lost and customer interruptions due to outages, where economically viable, opportunity is taken to automate the 11 kV distribution system by installing in line circuit breakers or actuators.

Circuits are generally prioritised for automation based on customer numbers and fault history.

#### **4.6 Auto Reclosers**

The majority of faults on overhead lines are of transient nature (e.g. insulator flash over) generally caused by wind borne materials. These faults are normally cleared by opening of the source circuit breaker or pole mounted recloser and do not recur when reclosed. Auto-reclosing is therefore applied to most predominantly overhead circuits.

Typical or preferred settings, where relays permit, are:

11 kV source circuit breaker:

- Trip 1 - Instantaneous high set overcurrent or time delayed overcurrent or earth fault or sensitive earth fault.
- 10 s dead time.
- Trip 2 - Instantaneous high set overcurrent or time delayed overcurrent or earth fault or sensitive earth fault.
- 10 s dead time (or lock-out if sensitive earth fault).

- Trip 3 - Time delayed overcurrent or earth fault.
- Trip 4 - Time delayed overcurrent and earth fault to lock-out.
- Reclaim time 5 s.

11 kV pole-mounted circuit breakers:

- Settings to co-ordinate with the above.
- Final dead time 140 s.

33 kV circuit:

- Single shot.
- 10-15 s dead time.
- 15 s reclaim time.

## **4.7 Operating Voltages**

### **4.7.1 General**

The company's distribution system operates at nominal voltages such as 33 kV, 11 kV and 230/400 V. Voltage control is applied at various voltage levels to ensure that statutory levels are maintained at customers' supply terminals as below.

### **4.7.2 Voltage Control of 11 kV and LV system**

Automatic control of the 11 kV source voltage is obtained by the on-load tapchanger on the 33/11 kV transformers. The interval between taps is typically 1.25%, 1.43 or 1.67%.

Line drop compensation is applied to some rural 33/11 kV transformer tapchanger control schemes to arrange automatic increase in the 11 kV source voltage with increase in demand. Typical settings are 1.05 p.u. at full load and 0.985 p.u. at no load. The 11 kV system is typically designed to accommodate 6% volt drop.

The low voltage system is typically designed so that the aggregate volt drop in the low voltage distributor and service does not exceed 7% with normally less than 2% in the service.


### **4.7.3 Voltage Control of 33 kV System**

Where appropriate the voltage at the 33 kV source is set to the highest permissible value, typically 1.03 p.u., in order to permit maximum design volt drop in the 33 kV system. It is also chosen to ensure that the required 11 kV and LV busbar voltages at both nearby and remote substations can be achieved.

## **4.8 Generation Connection Policy**

The principal duty placed on the authority is to protect the interest of consumers having regard to the need to secure that all reasonable demands for electricity are met. This duty is devolved to the licensee to develop the distribution systems in an economical manner whilst maintaining defined planning standards. The implications are that whereas demand for electricity must be met year round, generators will not always be able to simultaneously generate at their authorised capacity (generation is dispatched by the Transmission Operator) since the supply and demand for electricity must be balanced at all times. However, distribution connected generation is self dispatched and therefore networks have to provide firm access. Therefore, it is necessary that before any offer for connection is made, detailed network analysis is carried out to ascertain the impact of generation so that the quality of supply to connected consumers is not compromised.

Generators connected to the LV, 11 kV or 33 kV distribution system must comply with the general principles specified in Engineering Recommendation G98 or ER G99 as applicable. Where appropriate, the requirements of the Distribution Code and Grid Code must be met.



It is a requirement that Neutral Voltage Displacement will be fitted to all generators where the size of the generator or group of generators on the same connection point exceeds 200kVA. This is to ensure that the risks of back-energising the 11kV network from an LV generator is small.

Please also see section 4.10 - Network Constraints and Opportunities.

#### **4.9 Load Management Areas**

Due to the extent of SHEPD's unique geographic area, historic network and sparsely populated areas, there are several primary substations that are currently exempt from ER P2/7. This is because the solution to reinforce the network to meet ER P2 would not be co-ordinated, efficient and/or economic. These areas of the distribution network are governed by SHEPD's approved alternative planning standard.

The customer base at these sites is mainly domestic and the heating load is controlled by time switched regimes; these are managed to contain demands within circuit capability and to optimise utilisation.

#### **4.10 Network Constraints and Opportunities**

In accordance with its licence, SHEPD develops an efficient, coordinated and economical distribution system. However, our island networks present some additional challenges.

The distribution network in Shetland is not currently connected to any mainland distribution or transmission system. Supplies are provided from local generation using the 33 kV, 11 kV and LV systems.

The distribution system in Orkney is connected via 33 kV subsea circuits to the mainland distribution system. Security for the local distribution system is also currently provided by SHEPD owned local generation.

The distribution system supplying the Outer Hebrides is connected via 33 kV subsea cable and the security of supply is currently provided by SHEPD owned local generation.

Therefore, any application for large connection (demand or generation) in the above areas require careful evaluation so that voltage profile to customers, switchgear and plant fault level rating, subsea cable rating and stability of the system are not compromised.


SHEPD is committed to working with all parties looking to connect to its network to identify and deliver the best possible connection package for optimum benefit.

In particular, the continued growth in generation connecting at distribution voltages is driving ongoing improvements in how SHEPD seeks to provide information and assistance to customers wishing to connect to its network.

It is essential that prospective generation developers work with SHEPD to ensure correctly located and well-matched generation is incorporated into its network to the mutual benefit of both customers and the network.

Key areas that need to be discussed and monitored are the impacts of the generation on the network and the impacts of the network on the generation.

The addition of generation to the network impacts the system fault levels, which in turn can lead to network reinforcement works or other smarter solutions being necessary to support the connection. The power flows experienced by the modified network, if not accurately analysed, monitored and controlled, could cause system overload, over and under voltage, system frequency variations and reduce system power factors. All of these are undesirable on the distribution network.



Networks may have to be redesigned in order to best adapt to the generation connection requirement. This will add both cost and time to the connection project and should be considered and remembered when submitting any such connection enquiry or request.

Importantly, connection of well-sited and adaptable generation could provide network support and reduce network losses. The development must supplement SHEPD's responsibility to deliver a safe, secure and reliable network.

When considering connecting new load or generation to the network, it must be thoroughly planned and designed to meet the requirements set out in the Distribution Code, and in line with the information contained within this LTDS document.

The following short guide may assist users who wish to complete initial investigations and assessments of proposed connections to SHEPD's network."

#### Key Milestones in the initial connection investigation process.

Fill out a generation connection form, available from the ENA Website and submit this to SSEN: <https://www.energynetworks.org/operating-the-networks/connecting-to-the-networks>

This will commence dialog with the company in relation to the connection request. Identify your new Connection, Generation or Load.

- Decide on the capacity and type of generation to connect; Wind, Solar, Hydro, combined Heat and Power systems, Bio-mass or other.
- Unless a specific location is required, select an area on the LTDS geographic map or select a sub station local to the desired connection area.
- Using the information available in the LTDS investigate that the selected Substation's capacity, demand, forecast demand and fault level could support the new connection.
- Collect technical data from LTDS and perform self study.
- Carry out study to access the impact of new generation on the existing network parameters including;
  - Fault level contribution of connecting new generator?
  - Clean or dirty load giving rise to System harmonics?
  - Impedance of the unit, how will this alter fault level?
  - What is the effect under 1st circuit outage conditions?

Connection charges will vary with the location and size of the proposed connection. At the point of connection request or enquiry, costings will be advised in line with the SSEPD Statement of Methodology and Charges for Connection to SSEPD's Electricity Distribution System.

<http://www.ssen.co.uk/Library/ChargingStatements/SHEPD/>

Applications for connection of generation are evaluated on an individual basis. Information on generation connections and applications can be found in Table 5 and Table 6 of this statement's data section which summarises larger embedded generation installations in SHEPD's area.

#### 4.11 Transmission Constraints

Transmission capacity studies indicate that one of the main bottlenecks, termed the North-South constraint, for transferring power across the transmission system is between Kintore (near Aberdeen) and Tealing (near Dundee). This is due to high concentration of generation in the north and west. In general, new generation developments are difficult to locate without incurring significant expenditure on transmission reinforcement unless the new generation replaces existing generation.

In addition to the above there are other main import/export limitations in the south-west (Sloy-Inveraray), north-west (North of Beaulay) and north-east (Beaulay- Blackhillock).

Further information on constraints on the transmission system can be obtained in the Electricity Ten Year Statement, which is available on National Grid's Electricity System Operator website.

<https://www.nationalgrideso.com/>

SSEPD produce a Generation Availability map, which provides an indication of the networks capability to connect a large-scale development to a major substation.

The map can be viewed by following the link below:

<https://www.ssen.co.uk/generationavailability/>

## 5 GEOGRAPHIC AND SCHEMATIC PLANS

The following are included in this LTDS:

Schematic plans for the 33 kV system showing the electrical connectivity of the system.

Geographic map of the Network area.

Maps of 33 kV, 11 kV and LV systems for particular areas may be available on request depending on area. A price list for these is included in Appendix 1.

The distribution system of SHEPD interconnects with:

- The transmission system of Scottish Hydro Electric Transmission Ltd at the 132/33 kV substations shown in the schematic diagrams shown in the Electricity Ten Year Statement, which is available on National Grid's Electricity System Operator website. <https://www.nationalgrideso.com/>
- SP Energy Network's distribution systems at Strathleven & Abernethy 132/33 kV substations.

SP Energy Networks can be contacted via their website at:

<http://www.spenergynetworks.co.uk/>

The Distribution Code specifies the process for managing network development at interface point with users, which includes other Network Operators. It also describes the interface with the National Electricity Transmission System and SHEPD.



## 6 SOURCES OF NETWORK AND CHARGING INFORMATION

Charging Information is saved at:

<https://www.ssen.co.uk/Library/ChargingStatements/SHEPD/>

Competition in connections information is located at:

<https://www.ssen.co.uk/Connections/UsefulDocuments/>

Select “Competition in Connections” from the filter list.

SSEN Open Data Portal located at:

[SSEN Data Portal](#)



# DETAILED INFORMATION

## 7 OVERVIEW OF THE SYSTEM

### 7.1 Network Volumes

The following table shows the volume of SHEPD's distribution network.

<b>Voltage</b>			<b>Volume</b>
33 kV	Overhead Line	km	5355
	Cable	km	2322
	Transformers	33/11 kV and 33kV/LV	2800
11 kV	Overhead Line	km	20830
	Cable	km	5785
	Transformers	11 kV/LV ground and pole mounted	53791
Low Voltage	Overhead Line	km	3793
	Cable	km	11662

Table 2 – SHEPD Network Volumes

### 7.2 Network Data

The following data are included in this LTDS.

#### 7.2.1 Circuit Data

The electrical parameters for 33 kV circuits are shown in Table 1. All 33 kV circuits emanating from a grid substation are shown in a group. The circuit rating information relates to the main item i.e., cable or overhead line and is based on the smallest cross section. Cyclic ratings are given where appropriate. In practice other items such as current transformers, protection equipment and isolators may restrict the circuit rating. The information is intended to illustrate the basic circuit capability. The vast majority of circuits operate at their construction voltage.

#### 7.2.2 Transformer Data

33/11 kV transformer data is shown in Table 2. A site-specific analysis can be carried out to ascertain the reverse power capability of each transformer.

#### 7.2.3 Demand Data

The maximum demand recorded at the substation is shown in MW and power factor in Table 3. The forecast demand is based on our Distribution Future Energy Scenarios (DFES) projections, specifically the Consumer Transformation (CT) scenario. The DFES projections for 2022/23 are shown alongside the actual recorded values for a direct comparison. DFES projections for the next 5 years are shown where available, otherwise the forecast is based on the historical growth trend plus any large known developments. Firm capacity for multiple transformer sites relates to the remaining capacity under n-1 (largest unit loss), although higher loads can often be supplied by using load transfers or mobile or local generation. For single transformer sites the demand will normally be secured by use of interconnection, mobile generation or combination of both.

The minimum load scaling factor is the ratio of minimum to maximum demand.

Appendix 2 shows typical substation load profiles.

#### **7.2.4 Fault Level Data**

Calculated three phase fault level data under normal running arrangements at 33 kV and 11 kV nodes is shown in Table 4. There are some nodes which require a detailed network investigation before data is published. Normally there will be more than one circuit breaker at a substation site; the make and break ratings shown relate to the lowest rated circuit breaker. At most sites, not all circuit breakers would be subject to the fault currents given.

Fault currents given include contributions from all transmission and distribution networks and generation included in our study model. Making values include contributions from induction motors as set out in Engineering Recommendation G74.

The two fault currents published in this document are Peak Make and RMS Break. The Peak Make value has been calculated at a time of 10ms and includes both the AC and DC component of the fault current. The symmetrical RMS Break has been calculated at 60ms and includes the AC component of the fault current only. The associated X/R ratio is published and can be used to calculate the DC component of the fault. The asymmetrical RMS Break current is not published due to this value being dependent on site-specific components and settings.

Any fault levels calculated to within 95% of the circuit breaker rating at any given site will be highlighted before being assessed in further detail. Following the outcome of an additional study, steps to reduce fault level or reinforcement of switchgear may be proposed by SHEPD.

#### **7.2.5 Connected Generation**

A list of generation connected to SHEPD's distribution network is shown in Table 5. Standby and peak lopping generations are excluded from the table.

#### **7.2.6 Interest in a connection**

A high level summary of interest in demand and generation connections is shown in Table 6. 1MVA is the minimum installed capacity included in this table.

### **7.3 Other Information**

Additional information is available on request:

Circuits	e.g. zero sequence impedance.
Transformers	e.g. zero sequence reactance, earthing details, hot sites.
Demand	e.g. limitation on firm capacity, demand duration profiles.
Fault Level	e.g. contributions to fault current at each node, decremented break fault currents, details of limitations and indicative cost to relieve.

A price list for provision of such additional information is included in Appendix 1; contact details are in Part 1 Section 4.

## **8 NETWORK DEVELOPMENT PROPOSALS**

Appendix 3 lists financially approved distribution system reinforcement proposals. These schemes are either under construction or are in the design stage.

## 9 UPCOMING CHANGES TO THE FORM OF THE LTDS

On the 10<sup>th</sup> of January 2024, Ofgem opened the Formal Consultation for the LTDS reform, outlining proposed changes for how DNOs will produce and publish LTDS data moving forward. This reform intends to improve the usability of LTDS as DNOs are required to publish network models in Common Information Model (CIM) format, removing the need for customers to build models themselves. This consultation was followed up by a Formal Direction Letter published 30<sup>th</sup> of April 2024, which includes a suite of supporting documents including the new LTDS Form of Statement (FoS). SSEN are currently working on the staged implementation of the LTDS reform outlined by Ofgem. The below provides a summary of each stage of the LTDS reform and the associated timescales.

### **Stage 1: Existing Equipment (EQ) Model**

This stage requires DNOs to produce and publish a CIM Physical grid Model (EQ profile only) representing the existing grid of the entire licence area. While this stage will provide the EQ data within the model, users will still require the data from existing LTDS tables in order to run power flow and short circuit studies. EQ profiles are to be completed by 15 October 2024 and published in the November 2024 LTDS submission.

### **Stage 2: Existing & Future Equipment (EQ), Short Circuit (SC) and System Capacity (SYSCAP) Models**

This stage requires DNOs to produce and publish CIM Physical grid Models (EQ and SC profiles) representing the existing grid of their licence area accompanied by a SYSCAP profile Model. Data included at this stage includes historic peak load, system capacity, and fault level information. Models of the network representing each of five future years are also required at this stage. Models at this stage could provide sufficient data for a power flow study. Users could use this approach for both the existing network and for planned future changes reflected in future year models. This stage is planned to be completed by 15 April 2025 with models being published in the May 2025 LTDS submission.

### **Stage 3: Complete LTDS in CIM Grid Model Data with Solved Cases and Geospatial Location (GL) Model**

This stage is intended to provide geo-location of substations and circuits enabling understanding of the physical distance between a proposed development and the surrounding network. Schematic diagrams generated from, and related to, the underlying network model provide users with reliable visualisation of network data. Solved cases will allow users to validate their power flow calculations against our solutions, including information about future development projects or accepted-to-connect projects. This stage is planned to be completed by 15 August 2025 with models being published in the November 2025 submission.

The Solution Development Stages and LTDS publication cycle requirements are illustrated in the diagram below:

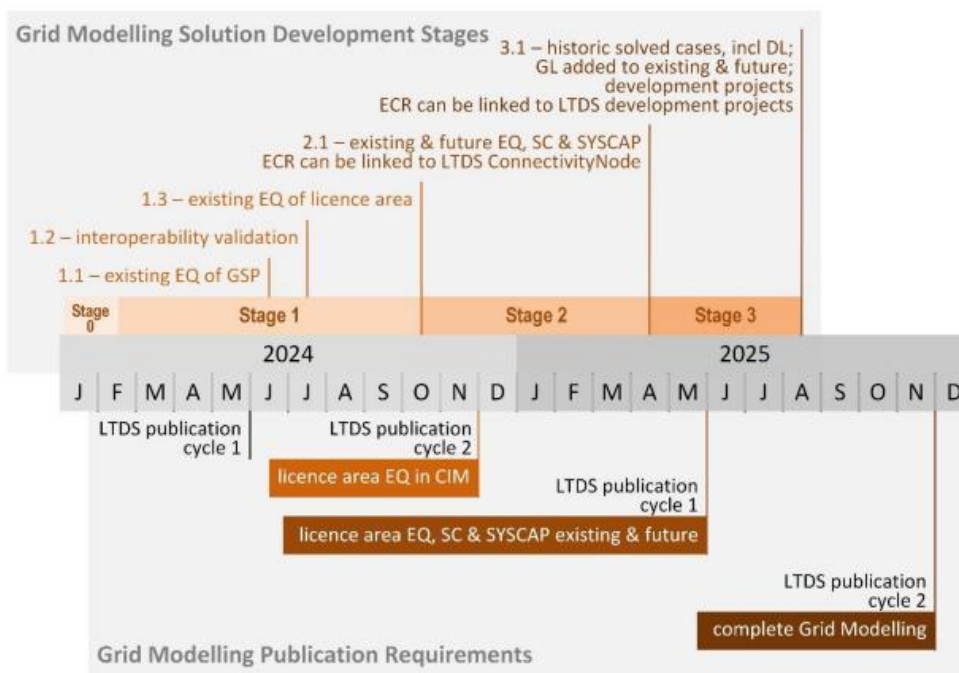


Figure 2 - LTDS Publication Cycle Requirements<sup>1</sup>

The current format of the LTDS is proposed to be retired over the staged implementation of the reform. The below table shows the proposed retirement dates of the existing LTDS Document and Data Tables. If these retirement timescales cause concern for your future use of the LTDS, please get in touch by emailing the SSEN Modelling and Reporting team at; [Modelling.Reporting@sse.com](mailto:Modelling.Reporting@sse.com).

Statement Section	Earliest Retirement Date
1.2.2 Detailed Information Section Content (other than schematic diagrams)	November 2025
3.2 Tables (entire subsection)	May 2025
Table 1 and 2	November 2024
Table 3, 4, and 5	May 2025
3.3 Decommissioned Assets	November 2024
4.1 Development Proposal Detail	November 2025
4.3 Interest in Connections (incl Table 6)	May 2025
7.1 File Format, Detailed Information subsection	November 2025
7.2 Frequency of Update and Availability, Detailed Information subsection	November 2025
7.2 Frequency of Update and Availability, Development Proposals - Development Proposal Detail subsection and Interest in Connections subsection	November 2025

Table 3 – Retirement of Existing LTDS Format : Proposed Timescales<sup>1</sup>

<sup>1</sup> Form of Long Term Development Statement ([ofgem.gov.uk](http://ofgem.gov.uk))

Further information on the proposed changes to the form of the LTDS can be found on OFGEM's website.

[Long Term Development Statement direction | Ofgem](#)

## 10 FURTHER INFORMATION

### 9.1 Distribution Code

See: [www.dcode.org.uk](http://www.dcode.org.uk)

### 9.2 Electricity Ten Year Statement

See: <https://www.nationalgrideso.com/>

### 9.3 Engineering Recommendations

Copies of National Engineering Recommendations and Technical Specifications are available from:

Energy Networks Association

6<sup>th</sup> Floor

Dean Bradley House

52 Horseferry Road

London

SW1P 2AF

Tel: 020 7706 5100

Email: [info@energynetworks.org](mailto:info@energynetworks.org)

or

[www.energynetworks.org](http://www.energynetworks.org)

# APPENDIX 1

## NETWORK INFORMATION PRICE LIST

SHEPD will be able to provide additional and/or site-specific network information on request. The price list given below is for general data which is normally available but will require time and effort to collect.

For some site-specific enquiries, and for those items that are not included in the list below, it may be necessary to carry out network analysis, site checks and in some cases shut down of the network to obtain information. A quotation will be provided to the customer before work is undertaken.

### Network Data

- a) **Reliability Data**
  - Typical reliability data for 33 or 11 kV and LV system £25 per voltage
  - Specific circuit reliability data £100 per circuit
- b) **Demand Data**
  - Specific demand (maximum and minimum) data - normal £100 per circuit running for 33 and 11 kV circuits
- c) **Impedance Data**
  - Specific 11 kV circuit impedance data £50 per circuit
  - Specific 33 kV circuit data additional to LTDS standard data £50 per circuit
- d) **Plant Data**
  - Rating, fault levels rating and protection details without site visit. (Where site visit is required, price will be provided on request) £100 per site

Any request for the above information should be sent in writing (see Part 1 Section 4 for contact details) including areas of interest showing details of the substation group and the substation or busbar node names and the information required. Under normal situations return of information will be within 15 working days.

### Geographic Mapping Information


Maps and network plans are available on request from SHEPD's Mapping Services department.

Mapping Services can offer access to our GIS mapping system information via the internet. This would allow repeated access at user's convenience. Requests for this service should be made directly to Mapping Services via email: [mapping.services@sse.com](mailto:mapping.services@sse.com)

This service may be subject to access and is provided free.

- One set of specific 33 kV system map with OS background £50 per printed set
- One set of specific 33 kV schematic diagrams £50 per printed set
- One set of specific 11 kV system map with OS background £50 per printed set
- One set of specific 11 kV schematic diagram Price on request

"One set of specific system mapping" Is defined as a 2km area centred as requested by the customer. This can be produced in either paper format or as a digital shape file or PDF.



In some cases, it will be necessary to obtain information from manufacturers or suppliers. SHEPD will use its best endeavours to obtain this but will not be held responsible for non- provision or delayed provision of such information. Any additional cost to provide such information will be advised.

Any request for the above information should be sent in writing accompanied with a cheque payable to Scottish Hydro Electric Power Distribution plc to:

Mapping Services  
Daneshill Depot  
Faraday Road  
Basingstoke  
Hampshire  
RG27 8QQ

Email: [asset.data@sse.com](mailto:asset.data@sse.com)

OR

Connections and Engineering  
Customer Service Centre  
Southern Electric Power Distribution  
Walton Park  
Walton Road  
Cosham  
Portsmouth  
PO6 1UJ

Email: [connections@sse.com](mailto:connections@sse.com)

**All prices are subject to VAT at current rates**

# APPENDIX 2

## TYPICAL 33/11 KV SUBSTATION LOAD PROFILES

The following box plots illustrate typical load profiles for 33/11kV Substations in Urban, Rural or Mixed environments.

Two sets of graphics for each environment are shown, a yearly profile and a daily profile, both derived from a Half Hourly dataset.

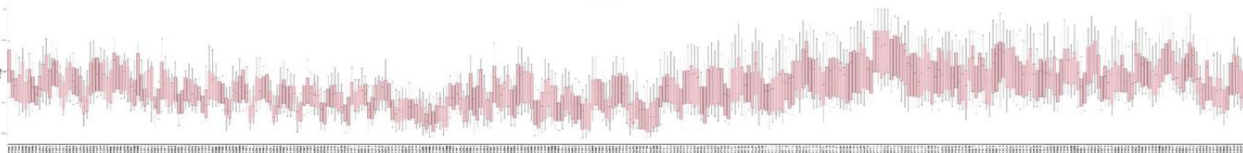
For the yearly graph, each box and whisker present a whole days' worth of half hourly data, illustrating the minimum and maximum for the day alongside the median and interquartile range.

For the daily graph, each box represents a specific half hour of the day, again illustrating the minimum and maximum for the day alongside the median and interquartile range.

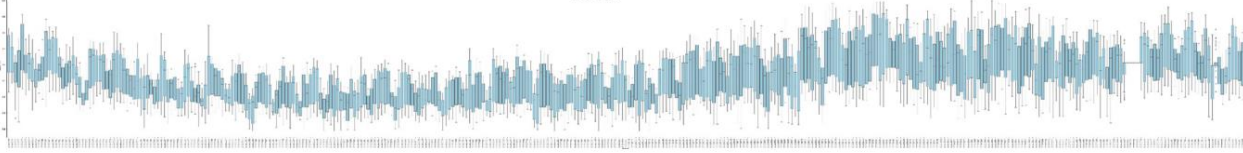
Yearly (1 April – 31 March) Half Hourly Data Box Plot



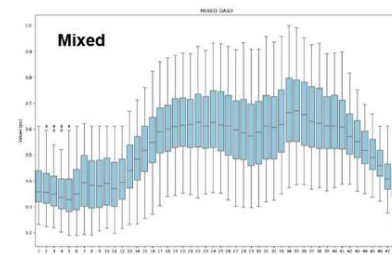
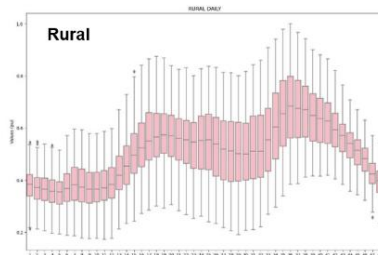
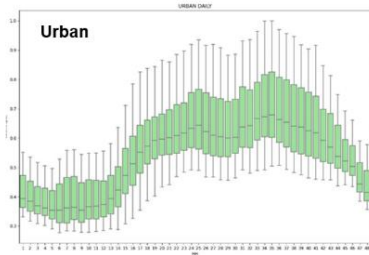
Yearly (1 April – 31 March) Half Hourly Data Box Plot



Yearly (1 April – 31 March) Half Hourly Data Box Plot



Daily (Midnight – Midnight) Half Hourly Data Box Plot





## APPENDIX 3

### NETWORK DEVELOPMENT PROPOSALS

GSP	Name	Estimated Completion	Impact on Distribution Network Capability	Changes from Nov 2023 Statement
Milton of Craigie	Longhaugh 33/11kV transformer Replacement	Completed	Increase in capacity Nodes: 84301 - 84304 & 84302 - 84304	Estimated completion changed from Dec-23
Milton of Craigie	Longhaugh 11kV switchboard Replacement	Completed	Increase in make and break fault ratings Nodes: 84304	Estimated completion changed from Dec-23
Abernethy	Errol 11kV switchboard Replacement	Completed	Increase in make and break fault ratings Nodes: 80013	Estimated completion changed from Oct-24
Scorradale	Stronsay 33/11kV Transformer Replacement	Jun-24	Increase in Transformer capacity Nodes: 86120	New
Dounreay	Dounreay 33kV Circuit Reinforcement	Jun-24	Fault level reinforcement	Estimated completion changed from Mar-24
Dyce	Circuit Reinforcement Dyce North	Aug-24	Increase in circuit capacity Nodes: 82419 - 82404, 82420 - 82405	Estimated completion changed from Mar-24
Strichen	Boddam 11kV Cable Reinforcement	Aug-24	Increase in circuit capacity - 84801	Estimated completion changed from Feb-24
Abernethy	Milnathort 11kV switchboard Replacement	Aug-24	Increase in make and break fault ratings Nodes: 80037	Estimated completion changed from Mar-24
Inverness	Inverness 33/11kV Transformer Replacement	Aug-24	Increase in transformer capacity Nodes: 83523	Estimated completion changed from Jun-24
Coupar Angus	Coupar Angus T2	Sept-24	Coupar Angus T2 was disconnected from network in May 2022 after it tripped the local protection. Coupar Angus T2 will be replaced with a 6.3MVA transformer. 81726	Estimated completion changed from Mar-24
Bridge of Dun	Logie Pert 11kV switchboard Replacement	Oct-24	Increase in make and break fault ratings Nodes: 80604	No change
Loch Carnan	Clachan 33/11kV Transformer Replacement	Oct-24	Increase in Transformer capacity - replace existing 2.5MVA transformer with 2 x 6.3MVA transformers Nodes: 84013	New
Craigiebuckler	Craigiebuckler 11kV Board Replacement	Nov-24	Ageing plant replaced with telecontrol. Increase in make and break fault ratings - 81800	Estimated completion changed from Jul-24

Taynuilt	Kinloch Isle of Mull (NoSR)	Dec-24	North of Scotland Resilience (NoSR) Increase in network security	Estimated completion changed from Dec-23
St Fergus	St Fergus Gas 11kV Board Replacement	Dec-24	Increase in make and break fault ratings Nodes: 21350	Estimated completion changed from Mar-24
Persley	Persley-Bridge of Don No1 & 2 33kV FFC replacement	Dec-24	Replace 33kV fluid filled cable with Al cables: change in cable capacity	Estimated completion changed from Oct-24
Dunoon	Bruchag 33/11kV Transformer Replacement	Dec-24	Increase in Transformer capacity - replace both 10MVA transformers with 7.5/15MVA transformers Nodes: 82222	New
Scorradale	Submarine Cable Replacement - Shapinsay/Mainland	Jan-25	Subsea cable replacement Nodes: 86121	Estimated completion changed from Mar-24
Scorradale	Eday 33/11kV Transformer Replacement	Feb-25	Increase in Transformer capacity - Replace both 10MVA transformers with 7.5/15MVA transformers Nodes: 86116	Estimated completion changed from Jun-24
Tummel Brudge	Errochty/Tummel Bridge Integration Works	Feb-25	Transfer 5 x 33kV circuits from Tummel Bridge 33kV switchboard to the new Errochty 33kV switchboard Nodes: 20130	New
Dyce	Balmedie P2 Compliance	Mar-25	Increase in network security 82416	Estimated completion changed from Dec-23
Port Ann	Primary Reinforcement - Glendaruel	Mar-25	Increase in transformer capacity Nodes: 84903 & 84907	Estimated completion changed from Dec-23
Thurso South	Spurness Reactor Replacement	Mar-25	Increase in Reactor size - from 2.5 to 4 DVAR solution Nodes: 86155	Estimated completion changed from Jun-24
Port Ann	Islay (NoSR)	Mar-25	North of Scotland Resilience (NoSR) Increase in network security	No change
Woodhill	Queens Lane North 11kV Board Replacement	Mar-25	Ageing plant replaced with telecontrol. Increase in make and break fault ratings 86403	No change
Milton of Craigie	Constable Street	Mar-25	Upgrading the transformers to 15/30 (CER) units, 82002	No change
Thurso South	Mount Pleasant 33/11kV Transformer Addition	Mar-25	Increase in network capacity - add a 2nd 7.5/15MVA transformer Nodes: 86011	New
Thurso South	Ormlie 33/11kV Transformer Addition	Mar-25	Increase in network capacity - add a 2nd 7.5/15MVA transformer Nodes: 86007	New
Tummel Brudge	Bonskied 33/11kV Transformer Replacement	Mar-25	Increase in Transformer capacity - replace existing 5MVA transformer with a 6.3MVA transformer Nodes: 86212	New

Gremista	Gremista 33kV outdoor c/b replaced with indoor switchroom	Apr-25	Ageing plant replacement; increase in make and break fault ratings	Estimated completion changed from Sep-24
Taynuilt	Taynuilt - Tullich 33kV Circuit Reinforcement	Apr-25	Increase in transformer capacity Nodes: 3L5: 19730-85917-85966 -85913; 6L5: 19730-85941-85964-85913	Estimated completion changed from Mar-24
Strichen	New Pitsligo 33/11kV Transformer Replacement	Jul-25	Increase in Transformer capacity - replace both 2.5MVA transformers with 6.3MVA transformers Nodes: 85802	New
Longman Drive	Longman Drive Substation	Nov-25	The proposed solution involves construction at both Longman Drive and Waterloo Primary substation (83519) with approximately 1.73km of dual 33kV cable linking both substations. The proposal for Longman Drive involves the building of a new indoor primary substation with associated transformers (2 x 12/24MVA) and switchgear (5 x 33kV & 10 x 11kV circuit breakers).	Estimated completion changed from May-24
Woodhill	Springhill 33/11kV Transformer Replacement	Mar-26	Increase in Transformer capacity - replace both 15/21MVA transformers with 20/40MVA transformers Nodes: 85107	New
Kintore	Methlick 33/11kV Transformer Replacement	Mar-26	Increase in Transformer capacity - replace T1 with a 6.3MVA transformer to match T2 Nodes: 83849	New
Dunoon	Rothesay 33/11kV Transformer Replacement	Mar-26	Increase in Transformer capacity - replace both 12/24MVA transformers with 7.5/15MVA transformers Nodes: 82218	New
Abernethy	Balbeggie 33/11kV Transformer Replacement	Mar-26	Increase in Transformer capacity - replace existing 5MVA transformer with a 7.5/15MVA transformer Nodes: 80005	New
Rannoch	Bridge of Gaur 33/11kV Transformer Replacement	Mar-26	Increase in Transformer capacity - replace existing 0.5MVA transformer with a 1MVA transformer Nodes: 85020	New
Battery Point	Battery Point 33kV Substation Replacement	Apr-26	The proposed works seeks to replace the three 4/8MVA transformers (85622) with two 15/30MVA. The works will also seek to replace both the 33kV and 11kV switchgear.	Estimated completion changed from Jun-24
Inverness	Culloden 33/11kV Transformer Replacement	Apr-26	Increase in Transformer capacity - replace both 15MVA transformers with 12/24MVA transformers Nodes: 83504	New

NEW	Rothienorman GSP Integration	May-26	Facilitate renewable generation/ DGEN reconfiguration to free up capacity at Keith & Kintore	Estimated completion changed from Mar-24
Elgin	Primary Reinforcement - Elgin	Mar-27	Increase in transformer capacity Nodes: 82513 & 82502	Estimated completion changed from Mar-25
Port Ann	Machrie T2 and 11kV switchboard Replacement	Mar-27	Additional 2.5MVA Tx to match existing unit and new indoor 11kV switchboard (25kV Break & 62.5kA Make) 81114	Estimated completion changed from Mar-25
Broadford	Kyle Primary - Replacement	Mar-27	New 33kV Substation - 5MVA Transformers to be increased to 6.3MVA. 80724 80725	Estimated completion changed from Jun-25
Keith	Roths 11kV & 33kV Switchgear Replacement	Mar-27	Increase in make and break fault ratings Nodes: 83608, 83609 & 83605?	No change
Keith	Insch 33/11kV Transformer Replacement	Mar-27	Increase in Transformer capacity - replace both 5/7.5MVA transformers with 7.5/15MVA transformers Nodes: 83630	New
Keith	Insch 11kV Switchboard Replacement	Mar-27	Increase in make and break fault ratings Nodes: 83630	New
Dyce	Kingseat 33/11kV Transformer Replacement	Mar-27	Increase in Transformer capacity - replace both 5MVA transformers with 7.5/15MVA transformers Nodes: 82409	New
Elgin	Ashgrove 33/11kV Transformer Replacement	Mar-27	Increase in Transformer capacity - replace T1 with a 12/24MVA transformer and add a 2nd matching transformer Nodes: 82513	New
Elgin	Bilbohall 33/11kV Transformer Replacement	Mar-27	Increase in Transformer capacity - replace T1 with a 12/24MVA transformer and add a 2nd matching transformer Nodes: 82502	New
Keith	Keith 2 33kV circuits	Mar-27	Increase in network security - Reinforce voltage compensation equipment at the new Glenrothes Distillery 33kV switchboard and loop into the 33kV ring Nodes: 83605, 83615 & 83618	New
Braco West	Creiff 33/11kV Transformer Replacement	Mar-27	Increase in Transformer capacity - replace both 7.5/15MVA transformers with 12/24MVA transformers Nodes: 80509	New
Burghmuir	Burghmuir 33kV circuits	Mar-27	Increase in network capacity - replace the Burghmuir to Inveralmond and Redgorton feeders Nodes: 80904 & 80926	New
Port Ann	Crinan 11kV switchboard Replacement	Mar-27	Increase in make and break fault ratings Nodes: 84915	Estimated completion changed from Mar-25

Lairg	Tressady Transformer Reinforcement	Apr-27	Increase in transformer capacity Nodes: 83904 - 83905	Estimated completion changed from Mar-24
Grudie Bridge	Achiltibuie - NOSR	Jul-27	New 11kV Interconnector	Estimated completion changed from Jun-25
Grudie Bridge	Ullapool Primary - T1 Replacement	Feb-28	Increase in Transformer capacity Nodes: 83324	Estimated completion changed from Apr-26
Thurso South	Lyness Primary - T1 Replacement	Feb-28	Increase in T1 transformer capacity to 1MVA Nodes: 86133	Estimated completion changed from Apr-26
NEW	Finstown GSP Integration	Mar-28	Facilitate renewable generation	Estimated completion changed from Mar-24
Thurso South	Sanday 33/11kV Transformer & Reactor Replacement	Mar-28	Increase in Transformer capacity Substation replacement - outdoor 33kV isolator arrangement to be replaced with indoor 33kV Switchboard alongside replacement of the reactor. 1.5MVA Transformer to be replaced with 2.5MVA. Nodes: 86118	Estimated completion changed from Jun-25 and description corrected (previously Spurness Reactor Replacement)
Loch Carnan	Drimore - NOSR	Mar-28	New network arrangement - 84005	Estimated completion changed from Jun-25
Braco West	Crieff 11kV switchboard Replacement	Mar-28	Increase in make and break fault ratings Nodes: 80509	No change
Tarland	Tarland Ring Reinforcement	Mar-28	Increase in network capacity - separate Aboyne Primary from the Tarland 33kV ring and establish a new primary substation in Braemar including 2 x 6.3MVA transformers Nodes: 86704 & 86708	New
Gremista	Scalloway - Setter Sandwick - Sumburgh Reinforcement	Mar-28	Increase in network security and increase transformer capacity - At Scalloway add a 2nd 8MVA transformer, at Setter Sandwick add a 2nd 8MVA transformer Nodes: 89972 & 89981	New
Keith	Keith 1 33kV circuits	Mar-28	Increase in network capacity - Reconfigure network with new circuit to Buckie, shed Cullen from ring and reinforce existing circuits Nodes: 83641 & 83645	New
Abernethy	Abernethy, Glendevon & Milnathort reinforcement	Mar-28	Increase in network capacity - Reconfigure the Milnathort/Glendevon 33kV network via the addition of 2 new 33kV circuits Nodes: 80033 & 80037	New

Redmoss	Newtonhill 33/11kV Transformer Replacement	Apr-29	Increase in Transformer capacity - replace both 15MVA transformers with 12/24MVA transformers Nodes: 85107	New
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The following projects have been cancelled since the November 2023 statement.

GSP	Name	Estimated Completion	Impact on Distribution Network Capability	Changes from Nov 2023 Statement
Grudie Bridge	Drumrunie Transformer Reinforcement	Cancelled	Increase in transformer capacity Nodes: 83331 - 83332	Cancelled
Grudie Bridge	Inverbroom Transformer Reinforcement	Cancelled	Increase in transformer capacity Nodes: 83320- 83321	Cancelled

The following assets have been decommissioned since the November 2023 statement.

GSP	Name	Asset Type	From PSSE Bus	To PSSE Bus
Milton of Craigie	Longhaugh	33/11kV Transformer (T1 & T2)	84301 & 84302	84304
Milton of Craigie	Longhaugh	11kV Switchboard	84304	N/A
Abernethy	Errol	11kV Switchboard	80013	N/A